

Fig. 2 Effect of nozzle geometry on correction factor.

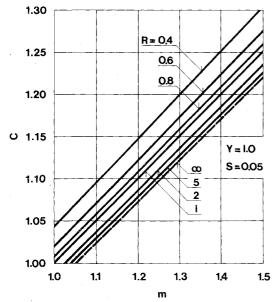


Fig. 3 Effect of temperature dependence of thermal conductivity on the correction factor.

and (9) are applied, the correction factor takes the form

$$C = \frac{S(m+1)(Y+R\cos\psi)}{2(R-S)(Y+S\cos\psi)} \left[\ln \frac{R(Y+S\cos\psi)}{Y(R-S)} \right]^{-1}$$
(10)

Geometrically similar expansion nozzles have identical correction factors if their temperature at corresponding points does not differ.

Discussion

As an example, the results for the particularly interesting nozzle throat (Y=I) are presented. In Fig. 2, C is plotted as a function of S with R as a parameter for m=1. It can be seen that for growing S the correction factor C deviates increasingly from the limiting case C=1. For expansion nozzles of rocket engines, $1 \le R \le 2$ and $S \le 0.05$ is generally recommended. In this range there is apparently no need for correcting Eq. (4) because the error is f < 1%. Recently, however, nozzle geometries approaching $R \ge 0.5$ have been discussed. The dashed line for $R \to \infty$ as a limiting case provides the correction factor for a tube.

Figure 3 shows correction factor C as a function of m for different values of R for Y=1 and S=0.05. This shows that frequently a correction of Eq. (4) becomes indispensable because the error reaches a percentage that cannot be tolerated even in approximate calculation.

References

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³Back, L.H., Massier, P.F., and Gier, H.L., "Convective Heat Transfer in a Convergent-Divergent Nozzle," *International Journal of Heat Mass Transfer*, Vol. 7, May 1964, pp. 549-568.

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Errata

Economical Scheme for Estimating Orbital Lifetimes

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ON page 324, Fig. 2 the curves labeled $e_0 = 0.7$ should be labeled $e_0 = 0.6$ and the curve labeled $e_0 = 0.60$ should be labeled $e_0 = 0.40$.

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Index category: Earth-Orbital Trajectories